

Strain Engineering for Functional Heterostructures: Aspects of Elasticity

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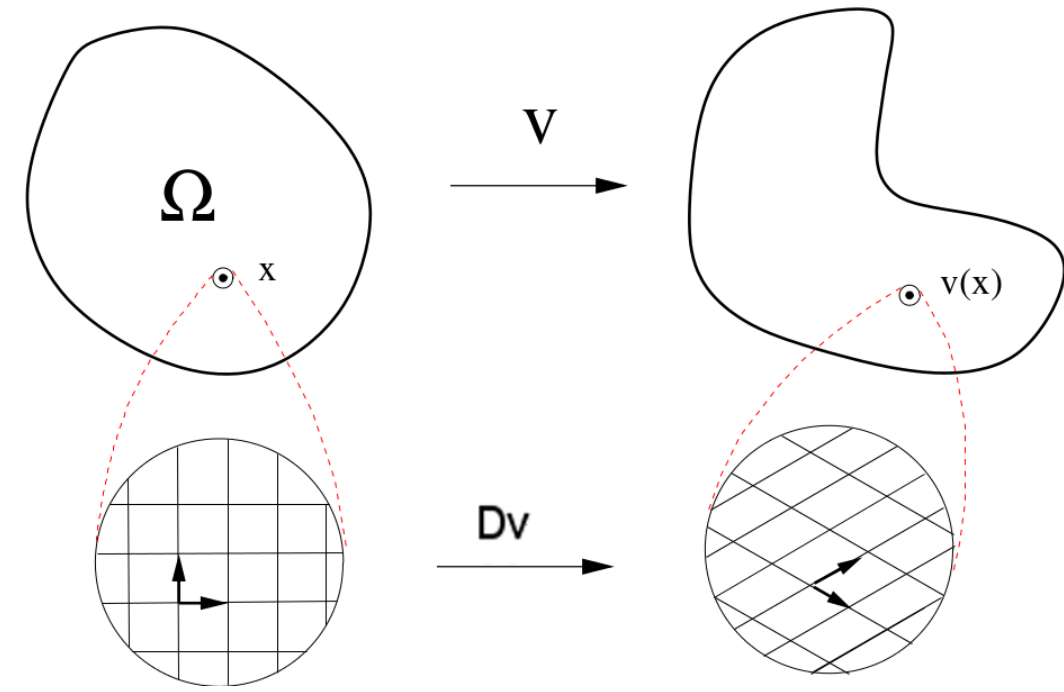
Summary

- Strain engineering for semiconductor devices or lithium-ion batteries requires a good understanding of elastic effects that strongly influence their functional properties
- Problems in the modeling of material systems related to:
 - Choice of free energy density with suitable properties
 - Dimension reduction for lower-dimensional structures
- In lower-dimensional structures, mathematical challenges arise due to the coupling of mechanical deformation with other physical effects such as electrostatics
- Use variational techniques, e.g., Γ -convergence, combined with modern tools for nonlinear partial differential equations

Polyconvex energy densities with generic elastic constants

Variational models of elasticity

- reference domain $\Omega \subseteq \mathbb{R}^n$
- deformation $v : \Omega \rightarrow \mathbb{R}^n$
- elastic energy $\int_{\Omega} W(\nabla v) dx \Rightarrow \min!$



Modeling assumptions for free energy density $W : \mathbb{R}^{n \times n} \rightarrow [0, \infty]$:

- frame invariance:** $W(RF) = W(F)$ for all $R \in SO(n)$ and all $F \in \mathbb{R}^{n \times n}$
- material symmetry:** For the point group $\mathcal{P} \subseteq O(n)$
 $W(P^T F P) = W(F)$ for all $P \in \mathcal{P}$ and all $F \in \mathbb{R}^{n \times n}$
- normalization:** $W(F) \geq 0$ and $[W(F) = 0 \iff F \in SO(n)]$
- existence of minimizers:** W polyconvex [Ball '77], i.e., there exists a convex and lower semi-continuous function $G : \mathbb{R}^{\tau(n)} \rightarrow [0, \infty]$ s.t.
 $W(F) = G(T(F))$, where $T(F) = (F, \det(F), \text{cof}(F), \dots)$
- linearization and measured elastic constants:**

$$\begin{aligned} W(\text{Id} + \varepsilon) &= W(\text{Id}) + DW(\text{Id})\varepsilon + \frac{1}{2}D^2W(\text{Id})[\varepsilon, \varepsilon] + o(|\varepsilon|^2) \\ &= \frac{1}{2} \sum_{ijkl} C_{ijkl} \varepsilon_{ij} \varepsilon_{kl} + o(|\varepsilon|^2) \end{aligned}$$

- smoothness and non-interpenetration:** $W \in C^\infty(\mathbb{R}^{n \times n})$ or $W \in C^\infty(\mathbb{R}^{n \times n} \cap \{\det > 0\})$ and $W(F) \rightarrow \infty$ as $\det F \rightarrow 0$

Typical approaches in the literature

- linear elastic energy density evaluated at nonlinear strains [?], which leads to non-polyconvex W
- specific ansatz using structural tensors \rightarrow restrictions on elastic constants

Result [Conti, Lenz & Zwicknagl, in preparation]:

Let P be a subgroup of $O(n)$, $\mathbb{C} : \mathbb{R}^{n \times n} \rightarrow \mathbb{R}^{n \times n}$ linear, symmetric s.t.

$$\begin{aligned} \mathbb{C}\xi : \xi &\geq \tilde{c}|\xi + \xi^T|^2, \quad \mathbb{C}(\xi - \xi^T) = \mathbf{0} \text{ for all } \xi \in \mathbb{R}^{n \times n}, \\ \mathbb{C}(R\xi R^T) : (R\xi R^T) &= \mathbb{C}\xi : \xi \text{ for all } \xi \in \mathbb{R}^{n \times n}, R \in P. \end{aligned}$$

Then,

(i) there is a polyconvex function $W \in C^\infty(\mathbb{R}^{n \times n}; [0, \infty))$ s.t.

$$W(\xi) \geq c \text{dist}^2(\xi, SO(n)), \quad \min W = W(\text{Id}) = 0, \quad D^2W(\text{Id}) = \mathbb{C}$$

and

$$W(QR^T\xi R) = W(\xi) \text{ for all } Q \in SO(n), R \in P, \xi \in \mathbb{R}^{n \times n}.$$

(ii) there is a polyconvex function $W \in C^\infty(\mathbb{R}^{n \times n} \cap \{\det > 0\}; [0, \infty))$ s.t. $W(\xi) \rightarrow \infty$ as $\det \xi \rightarrow 0$ and (i) holds.

Idea of the proof: Use linear elastic energy density evaluated at nonlinear strain near $SO(n)$, and construct explicit polyconvex extension using curvature of $SO(n)$.

Rigorous dimension reduction via Γ -convergence

Thin structures with thickness $0 < h \ll 1$

$$\text{plates } \Omega_h^{\text{plate}} = \omega \times \left(-\frac{h}{2}, \frac{h}{2}\right), \quad \omega \subset \mathbb{R}^{n-1}$$

$$\text{rods } \Omega_h^{\text{rod}} = (0, L) \times hS, \quad S \subset \mathbb{R}^{n-1}$$

Finite-strain electro-mechanical model for deformation v and electric potential φ

$$\begin{aligned} -\text{div}((\det M(x))\partial_F W(\nabla v M(x)^{-1})M(x)^{-T} - h^\alpha \text{div} \mathfrak{H}(\nabla^2 v)) &= 0, \\ -\text{div}(A(x, \nabla v)\nabla \varphi) &= q(x), \end{aligned}$$

- hyperstress regul. \mathfrak{H} leads to 2nd-grade nonsimple materials
- prestrain $M(x) \in \mathbb{R}^{n \times n}$ models lattice mismatch in heterostructures
- $A(x, F) = (\det F)F^{-1}a(x)F^{-T}$, $F = \nabla v$, is the pulled-back dielectric coefficient, $a \in L^\infty(\Omega_h)$ such that $a(x) \geq a_0 > 0$ a.e. in Ω_h , fixed charge density $q \in L^\infty(\Omega_h)$

System has saddle-point structure with energy functional

$$\begin{aligned} \mathcal{E}_h(v, \varphi) &= \mathcal{E}_h^{\text{mech}}(v) - \mathcal{E}_h^{\text{elec}}(v, \varphi) \\ &= \int_{\Omega_h} W(\nabla v M^{-1}) \det M + h^\alpha H(\nabla^2 v) + q\varphi - \frac{1}{2} A(\nabla v)\nabla \varphi \cdot \nabla \varphi dx \end{aligned}$$

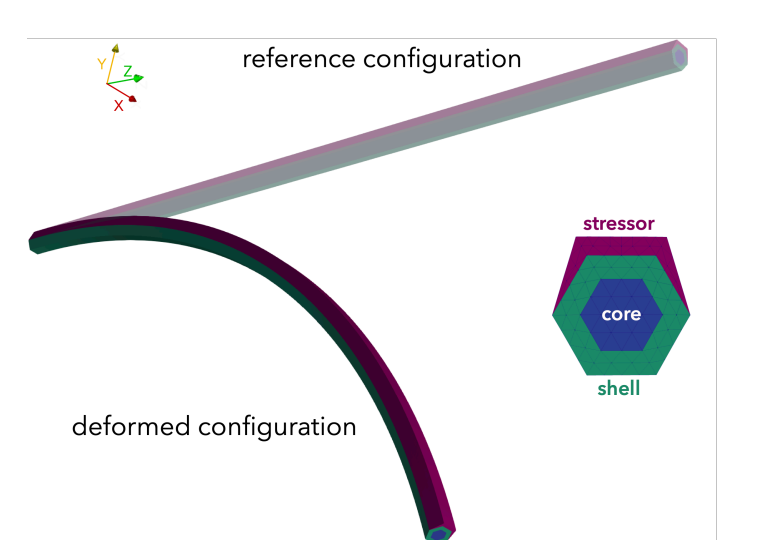
Work in progress: Limit passage for $h \rightarrow 0$ for thin plate in the bending regime, i.e., for the scaling $\tilde{\mathcal{E}}_h = \frac{1}{h^2}\mathcal{E}_h$ via Γ -convergence methods.

At the first stage, we have proved the Γ -convergence result for bending model with prestrain coupled by the Poisson equation without deformation, $\nabla v = \text{id}$, and with isotropic permeability.

Outlook: Investigate rod model and different scaling regimes.

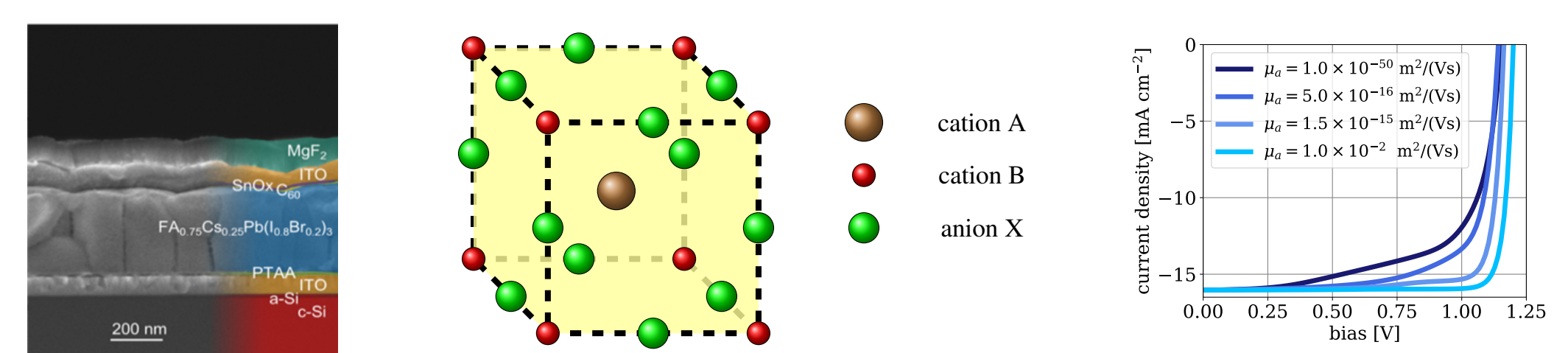
Strain distribution in zincblende and wurtzite GaAs nanowires

- mathematical model for heterostructures reacting on strain caused by lattice mismatch [?]
- non-linear elasticity with local prestrain
- simulations using finite element methods
- significant potential of strain to influence piezoelectricity and electronic band structure



Vacancy assisted charge transport (with PaA-1)

- Application: semiconductor/perovskite/semiconductor heterostructures for perovskite solar cells
- analysis of drift-diffusion models including the migration of ions: existence of weak solutions, boundedness [?], and uniqueness



Perovskite Silicon Tandem Solar Cell (Fraunhofer ISE, Freiburg), Perovskite unit cell, Current-Voltage-Characteristics

Cooperations

- S. Conti (Bonn), J. Ginster (WIAS), L. Abel (HUB), M. Rumpf (Bonn), M. Lenz (Bonn), Y. Hadjimichael (WIAS)
- AMaSiS 2024 workshop together with PaA-1, AA2-13, AA2-17
- Finite-strain hyperelasticity in battery models with PaA-2

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